

Effect of Soil- Structure Interaction on Response of Building Frame wit Piled-raft Foundation

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Abstract: The effect of soil structure interaction on response of the three storeyed (G+2) building frame supported on piled-raft foundation is reported in this paper. The three storeyed frame comprises of two bays and columns of the frames are supported by a piled-raft. The pile is assumed to be embedded in the cohesive soil mass. For the purpose of the analysis, simplified idealizations made in the theory of finite elements. The slab of the frame is idealized as two dimensional plate elements, beams and columns of the superstructure frame and pile of the sub-structure are idealized as the one dimensional bem-column elements. The soil mass is idealized by equivalent springs. The effect of different raft thicknesses with uniform pile diameter is evaluated on the response of superstructure through a parametric study. The response of the superstructure considered includes the displacement of the frame.

Keywords: Pile-raft, soil modulus, raft thickness, displacement

1. Introduction

The type of foundation and its design is based on the magnitude of the loads on it and the type of founding strata which supports it. If the founding stratum is within a reasonable depth, a shallow foundation in the form of raft is adequate. However, if the material is weak, the loads need to be transferred down to capable strata by means of deeper basements or piles. This is true, especially in case of multistoried building frames resting on weak sub soil strata where heavy structural loads acting on the frames have to be transmitted safely below to the firm strata.

The analysis of piled-raft foundation is very challenging because the load in the piled-raft structures is transferred to the soil not only by the interaction between the soil and the piles but also by the interaction between foundation structure and superstructure. In this interaction, deformations in the soils are the key factor which will affect forces and deformation in foundation and superstructure

In the past few decades, there has been an increasing recognition that the use of pile groups in conjunction with the raft can lead to considerable economy without compromising the safety and performance of the foundation. Such a foundation makes use of both the raft and the piles, and is referred to here as a *pile-enhanced raft or a piled raft*. The piled-raft concept has also proven to be an economical way to improve the serviceability of foundation performance by reducing settlements to acceptable levels. Although the piled-raft concept has been most notably applied to new construction involving high-rise buildings it is also potentially useful for remedial works and moderate height structures.

Methods that have been used for the analysis range from simplified calculations to numerical methods such as the boundary element method (Butterfield and Banerjee [1], Brown and Wiesner [2], Kuwabara [3], Mendonca and De Paiva [4]) and the finite element method (Hooper [5], Ottaviani [6], Chow [7], Liu and Novak [8], Katzenbach and Reul [9], Prakoso and Kulhawy [10], Reul and Randolph [11]). In early years because of the limited availability of computer memory and processing speed, the use of numerical methods was confined to simple problems. In last three decades due to rapid development in computer technologies, numerical methods such as full three dimensional finite element methods are often used to solve the complex problems.

The foundation concept of piled rafts differs from traditional foundation design, where the loads are assumed to be carried either by the raft or by the piles, considering the safety factors in each case. Several methods of analyzing piled rafts have developed over the years include approximation methods, finite element method, boundary element method, combined boundary element and finite element method, combined finite layer and finite element method; and variational approach.

2. Brief Review of Literature

In recent years, a variety of approaches for analyzing the piled- raft foundation system as mentioned in the preceding section have been developed over the years. All these approaches vary in the degree of sophistication of the formulations amount and the type of input parameters required, assumptions made; and in the applicability to realistic pile-soil-raft situations. Some of the significant studies are briefed approach wise in the subsequent paragraphs.

The approximation approach as presented by Chen *et. al.* [12] treated the raft as a thin plate, the piles as springs and the soil as an elastic continuum; and further, the interaction effects between the piles were ignored. Randolph [13] presented a method to compute the interaction between a single pile and a circular raft. Clancy and Randolph [14] employed a hybrid method in which analytical solution was combined with the finite elements. The raft was modeled by two-dimensional thin plate finite elements, the piles were modeled by one-dimensional rod finite elements and the soil response was calculated by using an analytical solution. Poulos [15] employed a finite difference method for the raft with the consideration of the interaction effects between the piles and raft. Kitiyodom and Matsumoto [16] developed a simplified method of numerical analysis using a hybrid model in which the flexible raft is modelled as thin plates and the piles as elastic beams and the soil is treated as springs.

The finite element method is one of the powerful tools for the analysis of the complex problems of piled raft. In order to reduce the computational efforts, the problems are sometimes simplified to an axi-symmetric problem or a plane- strain problem. Some of the noteworthy contributions using this method include those by Poulos *et al.* [17], and Sawant *et al.* [18]. Some of the researchers analyzed the circular piled rafts while few of them, reported the performance of piled raft foundation for a muti-storeyed building. Some of the analyses were carried out in the context of non-linear behaviour of soil; few of them even used finite elements in conjunction with infinite elements. While some investigations considered sandy soil, few of them considered the cohesive sub-soil. Even, a study considered layered soil. Some studies were carried out using complete three-dimensional finite element analysis; few studies were carried out in the context of simplified finite element models.

The boundary element method is a powerful tool that can be applied in engineering applications as only the boundary has to be discretized which reduces the amount of computer memory and the time to solve the problem as compared to that in finite element or finite difference method. This method provides a direct and accurate solution for the analysis. Moreover, it is fast and requires a moderate amount of computer storage space. The method has been used by many researchers (Brown and Wiesner [19], Kuwabara [20], Baziar *et al.* [21]) in the solution of the problem of piled raft embedded in different types of soil. Different idealizations were made for modelling different components of the foundation in question.

Based on the afore-mentioned review of literature, the analysis of a piled raft is presented using a software programme Build-Frame developed using FORTRAN 90. After assessing the accuracy of the programme in the context of simple problems of structural engineering and soil- structure interaction and further, implementing it on the published work, the said program is used in the present study. The present study aims at comparing the response of the piled-raft foundations with non-interactive, linear interactive and nonlinear-interactive analysis. The response of the frame included the displacement at each storey level of the frame along with the maximum positive and maximum negative bending moments in the individual beams and columns. A parametric study is carried out to examine the effect piled-raft on static nonlinear response with 0.5m thickness of the raft and 0.4 m pile diameter. The pile is assumed to be linear elastic throughout the analysis and soil is modeled using *von Mises* yield criteria.

3. Problem Description

A 3-D three storeyed building frame resting on piled-raft foundation is considered for the study. The frame, 3 m high is 10 m \times 10 m in plan with each bay being, 5m \times 5m. The slab, 200 mm thick, is provided at top as well as at the floor level. The slab at the top of the first, second and third storey is supported over 300 mm wide and 400 mm deep beams. The beams are resting on columns of size 300 mm \times 300 mm. While dead load is considered according to the unit weight of the materials of which the structural components of frame are made up of, for the purpose of the parametric study presented here. The properties of the material for pile and pile cap are given in Table 1.

Table 1. Pile-raft and soil	properties for	parametric study
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Soil properties				
Modulus of Elasticity, E_{s}	20000 kPa			

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Poisson's ratio, μ 0.4 18 kN/m³ Density, γ_s 100 kPa Yield stress, σ_v **Interface element** $1.0 \times 10^{6} \text{ kN/m}^{3}$ Normal stiffness, *K*_n Tangential stiffness, K_s 1000 kN/m **Piled-raft properties** Modulus of Elasticity, E 25 GPa Poisson's ratio, μ 0.2 Density, γ_p 25 kN/m³



(a) Building frame with fixed base-half symmetry

(b) Building frame with piled-raft

Fig.1 Building frame considered in the present study

The schematic of the building frame with fixed base-half symmetry and piled-raft is shown in Fig. 1 (a) and (b). While dead load is considered according to unit weight of materials of which the structural components of frame are made up for the parametric study presented here, a

lateral load of 1000 kN is assumed to act at joints of the frame. The analysis carried out in the context of linear behavior of soil is extended further to account for the non-linearity of the soil using von Mises yield criterion.

3.1 Effect of Pile Diameter on Storey Displacement

The values of the horizontal displacement at each storey level of the frame with the pile spacing in respect of four diameters of the pile (400, 600, 800 and 1000mm) considered in the study is shown in Table 2. The corresponding percentage increase in displacement due to consideration of SSI (linear-interactive w.r.t. non-interactive, i.e., fixed base, and further, non-linear-interactive w.r.t. linear-interactive) is indicated in brackets in Table 2. Similarly, the variation in the storey displacement with storey height in respect of different raft thicknesses (2.05m, 0.5m, 0.75m, 1.0m, 1.25m and 1.50m) considered in the present investigations is shown in Fig. 6.2.

	Raft thickness = 0.25 m					
Pile diameter (mm)	Storey Height (m)	9.0	6.0	3.0	0.0	
	Analysis	Displacement (mm)				
	Non-interactive	363.99	294.9	162.53	0.0	
400	Linear	412.23	324.25	198.11	11.02	
		(13.25 %)	(9.95 %)	(21.89 %)	(100 %)	
	Nonlinear	411.02	333.45	185.60	12.23	
		(12.92 %)	(13.07 %)	(14.19 %)	(100 %)	
600	Linear	409.81	319.01	190.20	10.87	
		(12.59 %)	(8.18 %)	(17.02 %)	(100 %)	
	Nonlinear	395.24	322.46	175.25	12.12	
		(8.59 %)	(9.35 %)	(7.83 %)	(100 %)	
800	Linear	402.42	302.22	181.78	10.56	
		(10.56 %)	(2.48 %)	(11.84 %)	(100 %)	
	Nonlinear	388.25	312.45	171.25	12.03	
		(6.67 %)	(5.95 %)	(5.37 %)	(100 %)	
1000	Linear	397.65	299.45	175.23	10.02	
		(9.25 %)	(1.54 %)	(7.81 %)	(100 %)	
	Nonlinear	378.99	303.63	164.99	11.23	
		(4.12 %)	(2.96 %)	(1.51 %)	(100 %)	

Table 2 Effect of pile diameter on storey displacement for raft thickness 0.25 m.

The general trend observed for all the pile diameters considered in this investigation is that horizontal displacement at each storey level increases due to the effect of soil structure interaction (SSI). It is seen that the displacement at top of each storey is on higher side corresponding to four different pile diameters (400, 600, 800 and 1000 mm) considered in the present investigation when compared with the values of top displacement obtained in non-interactive analysis.

The reduction in the displacement is attributed to the improved passive resistance of soil with higher pile diameter. The general trend observed for all the pile diameters considered in the investigation in respect of all the pile diameters is that horizontal displacement is more when the diameter is less and thereafter, decreases with higher value of pile diameter considered in present study.

From the results of parametric study conducted on a specific building frame with piled-raft foundation of 0.25 m thickness, the displacement at each storey level is found to be very less (Non-interactive) when the column bases are assumed to be fixed and increase owing to interactive analysis, i.e., when the effect of soil-structure interaction is taken into account. The displacement is observed to be maximum at the top of the frame, i.e., third storey. The maximum value of top storey are found to be 412.23 mm, 409.81 mm, 402.42 mm and 397.65 in respect of various pile diameters considered in the present investigation for the pile diameters 400 mm, 600 mm, 800 mm and 1000 mm, respectively. The interactive analysis is found to increase the storey displacement in the range of 9.52 – 13.25 %, 1.54 – 9.95 %, and 7.81 – 21.89 %, respectively at first, second and third storey level. Further, it is seen that the increase in displacement due to consideration of SSI is prominent on the bottom storey for any pile diameters and with increase in the storey; the increase in displacement goes on decreasing. Similar trend is observed in respect all raft thickness considered in the present investigation.

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Fig 2: Effect of pile diameter on storey displacement for raft thickness 0.25 m.

4. Conclusions

From the parametric study presented in this paper, following significant conclusions can be drawn:

- The effect of soil- structure interaction on each storey displacement of the frame is quite significant. Displacement is less for the conventional analysis and increases when nonlinearity of soil is considered.
- With increase in pile diameter, storey displacement decreases in respect of all pile dimeters considered in the study. A displacement for minimum raft thickness and higher value of soil modulus is on higher side.
- It is seen that the displacement at top of each storey is on higher side corresponding to four different pile diameters considered in the present investigation when compared with the values of top displacement obtained in non-interactive analysis

All the same, the effect of soil-structure interaction (linear and nonlinear) is shown to be prominent on the response of the specific building frame considered and the type of foundation used in the present study.

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