International Research Journal of Engineering and Technology (IRJET) Volume: 06 Issue: 04 | Apr 2019 www.irjet.net

e-ISSN: 2395-0056 p-ISSN: 2395-0072

# **Design and Analysis of Residential Building**

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**Abstract** - This Project is Generally Based on Theoretical Design And Analysis of structural framed building. Planning, Analysis and design of G+4 residential building structure by using IS-Code method, manually designed and over verifies by using software. Planning of any types of building is done by national building code (NBC) in India, Hence the residential building is properly planned in accordance with the national building code of India. The reinforced concrete framed structure consisting of G+4 with adequate facilities. All the structure member are designed using limit state method with reference of IS:456-2000. Different load active on the member (beam, column) are considered according to the code IS:875(part1,part2,part3).

#### *Key Words:* Residential Building, Staad-pro V8i Analysis, Multi-stories Building, Design and Analysis of Framed Building, NBC.

# **1. INTRODUCTION**

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Now a days due to overpopulation and high cost of land, multi-storied building is more essential for metropolitan city. Multi-storied Residential building is the perfect solution for living of high populated area. A multi-storied building, which posses multiple floor above the ground level, which aim to increase the floor area of building in shortest built up area.

Structure analysis is a subject which involves designing, planning to built up a perfect building. Basically each project are different with their design criteria such as incoming load, soil properties, dynamic load, built up area etc. Here we provided the details to complete a residential apartment theoretically.

We firstly collected some required data to measure the soil specific such as moisture content, bearing capacity of soil, types of soil etc. We provided the perfect parameter in beam, slab, column and footing with the consideration of incoming load to avoid shear and bending collapse. In accordance with limit state method of collapse in IS-456:2000 we built G+4 building which deal with strength and stability of structure under maximum design load flexure, compression, shear and torsion.

#### **2. LETARATURE REVIEW:**

**P.P. Chandurkar et. al. (2013): Study of G+9 building:** Had presented study of G+9 building having three meters height for each storey. The whole building design had carried out according to IS code for seismic resistant design and the building had considered fixed at base. Structural element for design had assumed as square or rectangular in section. They had done modelling of building using ETAB software in that four different models were studied with different positioning of shear walls.

# Mohit Sharma et.al. (2015): To study the dynamic analysis of multi-storeyed Building:

He considered a G+30 storied regular reinforced concrete framed building. Dynamic analysis of multi-storeyed Building was carried out. These buildings have the plan area of 25m x 45m with a storey height 3.6m each and depth of foundation is 2.4 m. & total height of chosen building including depth of foundation is 114 m. The static and dynamic analysis has done on computer with the help of STAAD-Pro software using the parameters for the design as per the IS:1893-2002 Part-1 for the zones- 2 and 3. It was concluded that not much difference in the values of Axial Forces as obtained by static and dynamic analysis.

# M. S. Aainawala et. al. (2014): Comparative study of multi-storeyed R.C.C. Buildings with and without Shear Walls:

He did the comparative study of multi-storeyed R.C.C. Buildings with and without Shear Walls. They applied the earthquake load to a building for G+12, G+25, G+38 located in zone II, zone III, zone IV and zone V for different cases of shear wall position. They calculated the lateral displacement and story drift in all the cases. It was observed that Multistoreyed R.C.C. Buildings with shear wall is economical as compared to without shear wall. As per analysis, it was concluded that displacement at different level in multistoreyed building with shear wall is comparatively lesser as compared to R.C.C. building without shear wall. Which is important for building design and use of shear walls.

**M. Mallikarjun et. al. (2016): on analysis and design of a multi-storied residential building of ung-2+G+10:** Carried study on analysis and design of a multi-storied residential building of ung-2+G+10 by using most



economical column method and the dead load and live load was applied on the various structural component like slabs, beams and found that as the study is carried using most economical column method this was achieved by reducing the size of columns at top floors as load was more at the bottom floor. The economizing was done by means of column orientation in longer span in longer direction as it will reduce the amount of bending and the area of steel was also reduced.

# **3. METHODOLOGY**



# 4. WORK PROGRESS

# **4.1 BASIC DATA**

i. Type of building – Residential building.

ii. Type of structure – multi storey rigid jointed framed

iii. No. of storey – 5 (G+4)

iv. Floor to floor height – 3.04 m.

v. External walls – 230 mm including plaster

vi. Internal walls – 150 mm inculing plaster vii. Bearing capacity of soil – 200 KN/m<sup>2</sup>

viii. Height of plinth – 0.6 m.

**NOTE**:-Others required data assume using NBC(national building code) for planning and IS:456-2000 for concrete design work.

# 4.2 PLAN OF RESIDENTIAL BUILDING



Fig1: Plan of Residential Building.

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# 4.3 DESIGN OF BUILDING COMPONENTS

# **DESIGN OF SLAB**

#### Given data :

Lx = 3.36 m Ly = 3.89 m

Ly/Lx = 1.16 < 2 hence it's a two way slab

Live load =  $2 \text{ KN/M}^2$ , Floor finish =  $1 \text{ KN/M}^2$ 

M. Factor = 1.3 [For HYSD]

L/d = 28 x M.F. =>3360/d = 28 x 1.3

d = 92.30mm.

Assume D=140mm and d=120mm.

#### Effective span :

Width of the support = 230mm

Clear span = 3360 + 230 = 3590 mm

1/12 x 3590 = 299.16 mm > 230 mm

 $L_y = 3590 \text{ mm} \& L_x = 4120 \text{ mm}$ 

#### Load calculation:

Self-weight of slab =  $0.140 \times 25 = 3.5 \text{ KN/M}^2$ 

Live load =  $1 \text{KN}/\text{M}^2$  Floor finish =  $2 \text{ KN}/\text{M}^2$ 

Ultimate load = 1.5 x 6.5 = 9.75 KN/M<sup>2</sup>

#### Moment calculation:

 $M_x = \alpha_x x w x l_x^2 \qquad \qquad M_y = \alpha_y x w x l_x^2$ 

 $L_y/L_x = 1.15$  [From table 26 page- 91 IS 456 ;2000 ]

$$\alpha_{\rm x} = 0.079$$
 &  $\alpha_{\rm y} = 0.060$ 

M<sub>x</sub> = 0.079 x 9.75 x 4.12<sup>2</sup> = 13.075 KN.M

 $M_v = 0.060 \ge 9.75 \ge 4.12^2 = 9.93 \text{ KN.M}$ 

#### Check for flexure:

d<sub>x</sub> provide = D -15 -10/2 = 120 MM

 $d_y$  provide = d - 10/2 = 115 MM

 $Mu = Mu_{limit}$ 

 $13.075 \ge 10^6 = 0.14 \ge 20 \ge 1000 \ge d^2$ 

 $d_{required.}(68.33 \text{ mm}) < d_{provided}(120 \text{ mm}) :: Hence safe in flexure}$ 

#### **Reinforcement calculation:**

Ast<sub>x</sub> =  $\frac{0.5 \times 20}{415} \left( \sqrt{1 - \frac{4.6 \times 13.075 \times 106}{20 \times 100 \times 120 \times 120}} \right)$  120 x 1000 = 319.59 mm<sup>2</sup>

International Research Journal of Engineering and Technology (IRJET) e-ISSN: 2395-0056 IRJET Volume: 06 Issue: 04 | Apr 2019 www.irjet.net

p-ISSN: 2395-0072

Spacing along X direction-

 $=\frac{\text{Area of 1 bar x 1000}}{\text{Astx}} = \frac{\frac{\pi}{4} \times 100 \times 1000}{319.59} = 245 = 220 \text{ mm say}$ 

Provide 10 mm  $\phi$  @220 mm c/c.

Ast<sub>y</sub>=  $\frac{0.5 \times 20}{415} \left( \sqrt{1 - \frac{4.6 \times 9.93 \times 106}{20 \times 100 \times 120 \times 120}} \right)$  120 x 1000 = 239.20 MM<sup>2</sup>

Spacing along Y direction-

 $=\frac{\text{Area of 1 bar x 1000}}{\text{Astx}} = \frac{\frac{\pi}{4}x 100 x 1000}{239.20} = 328 = 300 \text{ mm say}$ 

::Provide 10 mm $\phi$  300 mm c/c.

#### **Check for shear:**

$$V_{u} = \frac{Wu \times Lx}{2} = \frac{9.75 \times 3.59}{2} = 17.50$$
$$T_{u} = \frac{Vu}{bd} = \frac{17500}{120 \times 1000} = 0.145 \text{ N/M}^{2}$$

 $T_{cmax} = 2.8 \text{ N/M}^2$  [Page = 63 Table – 20 IS 456 :2000]

 $Pt\% = \frac{Ast}{bd} \times 100 = \frac{319.59}{120 \times 1000} \times 100 = 0.266$ 

 $T_c = 0.36 \text{ N/M}^2 < T_{cmax}$ ::Hence safe in shear .

#### **Reinforcement in edge strip:**

 $A_{st}$ = 0.12/100 x 1000 x 140 = 168 mm<sup>2</sup>

Spacing = 299 = 280 mm say

::Provide 8 mm  $\phi$  @ 280 mm c/c.

#### **Torsion reinforcement at corners:**

Maximum middle strip Reinforcement = 357mm<sup>2</sup>

Reinforcement each of the four layer =  $\frac{34}{4} \times 357 = 267.75$ mm<sup>2</sup>

Ast in each layer at each corner where one edge is discontinuous = 0.50 x 267.75 = 133.87 mm<sup>2</sup>

Length of bars = Lx/5 = 3590/5 = 718 = Say 720 mm.

#### **DESIGN OF BEAM**

#### Given data :

Length (L) = 5.50 MWidth (b) =0.230 M

Depth cover (d') = 35 MM

Grade of Concrete ( $F_{ck}$ ) = 20 N/MM<sup>2</sup>

Grade of steel ( $F_v$ ) =415 N/MM<sup>2</sup>

#### Load calculation:

L/d = 20[page -37 clause-23.2.1,IS:456-2000]

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d=5500/20 = 275 :: Provide D = 600 MM. & d =(600-35)=565 MM. Self-weight of beam = 25 x .23 x.38 = 2.185 KN/M<sup>2</sup> Self-weight of wall = 19 x .23 x 2.66 =11.62 KN/M<sup>2</sup> Total Incoming load on beam from slab. Self-weight of slab =  $25 \times 0.1 = 2.5 \text{ KN/M}^2$ Live load =  $2KN/M^2$ , Floor finish =  $1 KN/M^2$ Total load = 5.5 x Area of slab = 5.5 x 4.184 = 23.012 KN.  $\tan 45^{\circ} = h/b => h = 3.59/2 = 1.8 M.$ Area of section 1 & 2 =  $\frac{1}{2}$  x 1.8 x 1.8 = 3.23 M<sup>2</sup> Area of section  $3 \& 4 = 3.23 + (4.12 - 3.59) \times 1.8 = 4.184 M^2$ Point load concrete due to Beam = 8.395 KN/M. Load from Slab =  $(5.5 \times 0.515) = 3.22 \text{ KN/M}$ . Total load on beam = (23.012 + 3.22) = 26.23We can assume 1 M length of beam. Total length of beam = 5.50 M Total load = (26.23/5.50 + 2.185) = 6.95 KN/M Ultimate total = (6.95 + 11.62 + 8.395) = 27.26 KN/M Ultimate load = (1.5 X 27.26) = 40.99 KN /M Moment calculation:  $M_u = (W_u \times L_{eff}) / 8 = 40.9 \times 5.50^2 / 8 = 154.64 \text{ KN.M}$ **Check for flexure:**  $M_U = M_{ulimit} = 154.64 \text{ x } 10^6 = 0.14 \text{ x } 20 \text{ x } 230 \text{ x } d^2$ d = 490 < d(provided) = 565 mm

:: Safe in flexure.

#### **Reinforcement calculation:**

Ast = 
$$\frac{.5 \times 20}{20} \left( \sqrt{1 - \frac{4.6 \times 154.65 \times 1000000}{20 \times 230 \times 565 \times 565}} \right) 230 \times 565 = 882.910$$

 $MM^2$ 

:: No of bars required of 16 mm dia. =  $\frac{882.91}{\frac{\pi}{5} \times 16 \times 16}$  = 4.39 = 5 say

Provide 5# 16 mm diameter.

#### Check for shear:

 $V_u = \frac{Wu \times L}{2} = \frac{40.9 \times 5.50}{2} = 112.475 \text{ KN}$  $T_u = \frac{Vu}{bd} = \frac{112475}{230 x 565} = 865.5 \text{ N/MM}^2$ 

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T <sub>cmax</sub> = 2.8 [ page 73 table 19 IS:456-2000 ]	WALL,			
$::T_u < T_{cmax}$ :: Hence ok.	Wt. of internal walls = [0.152 x (3.04 – 0.380) x19]			
$P_{t06} = \frac{Ast}{2} \times 100 = \frac{5 \times \frac{\pi}{4} \times 16 \times 16}{2} \times 100 = 0.774$	=7.68KN/M <sup>2</sup>			
$\frac{100}{bd} = \frac{100}{230 \times 565} \times 100 = 0.774$	Ultimate load = $(1.5 \times 7.68) \text{ KN/M}^2$			
Tc = 0.56 [ page 73 Table-19 IS:456-2000]	=11.52KN/M <sup>2</sup>			
:: Hence safe in shear.				
Minimum shear reinforcement:	<u>MAIN BEAM,</u>			
$Sv = \frac{0.87 \times 415 \times 2 \times \frac{\pi}{4} \times 36}{2} \times 565 = 290.54 \text{ mm}^2$	Size of Beam = (230 x 450)mm			
$5y = 112475 - 0.56 \times 230 \times 565^{\circ} = 2.90.5 + 11111$	Wt. of Beam = [0.230 x (0.450 – 0.140) x 25]			
Minimum spacing:	= 1.78KN/M <sup>2</sup>			
$Sv = \frac{0.87 \times 415 \times 56.54}{0.4 \times 230} = 221 \text{mm}.$	Ultimate load = $(1.5 \times 1.78) \text{ KN/M}^2$			
:: Provide 2 legged 6 mm diameter @ 220mm c/c .	=2.67KN/M <sup>2</sup> SECONDARY BEAM,			
:: Size of the beam (9"X24")	Size of Beam = (230 x 380)mm			
DESIGN OF COLUMN	Wt. of Beam = $[0.230 \times (0.380 - 0.140) \times 25]$			
Given data:	$= 1.38 \text{KN}/\text{M}^2$			
<u>ROOF,</u>	Ultimate load = $(1.5 \times 1.38)$ KN/M <sup>2</sup>			
Live load = 2KN/M <sup>2</sup>	=2.07KN/M <sup>2</sup>			
Floor Finishing = 1KN/M <sup>2</sup>	Ultimate load = 1.5[( 0.23 X 0.40) X 25]			
FLOOR.	$= 3.9675 \text{ KN/M}^2$			
Live load = $4$ KN/M <sup>2</sup>	Total secondary beam load = $6.0375$ KN/M <sup>2</sup>			
Floor Finishing = 1KN/M <sup>2</sup>	Floor Area Transferring Load On Column			
Load calculation:	= (3.515 x 3.10)			
<u>ROOF</u> ,	$= 10.89 m^2$			
Live load = $2KN/M^2$	• Length Of Walls = $(2.90 - 0.38)/2 + 3.21/2$			
Self-wt. of slab = 0.140 x 25 =3.5 KN/M <sup>2</sup>	-2.0011			
Floor finish = 1KN/M <sup>2</sup> Total Load = 6.5KN/M <sup>2</sup>	• Length of Main Beam = $(2.90 - 0.36)/2 + 2.47/2$ = 2.495m			
Ultimate load = $(1.5 \times 6.5) \text{ KN}/\text{M}^2=9.75\text{KN}/\text{M}^2$ <u>FLOOR</u> ,	<ul> <li>Length Of Secondary Beam = 2 x (3.12/2) = 3.21m</li> </ul>			
Live load = $4KN/M^2$	Load on column in kN :			
Floor finish = 1KN/M <sup>2</sup>	1. <u>Roof &amp; 4<sup>th</sup> Floor</u> :-			
Self wt. of slab = $0.140 \ge 25 = 3.5 \text{ KN/M}^2$	• Roof slab = $10.89 \times 9.75$ = $106.17 \text{ KN}$			
Total Load = $8.5 \text{KN}/\text{M}^2$	• Walls = $2.86 \times 11.52 = 32.95 \text{ KN}$			
Ultimate load = $(1.5 \times 8.5) \text{ KN/M}^2$	<ul> <li>Main Beam = 2.495 x 4.71 = 11.75 KN</li> <li>Secondary Beam = 3.21 x 6.0375 = 19.38</li> </ul>			
=12.75KN/M <sup>2</sup>	KN Total Load = 170.25 KN			
	2. 4 <sup>th</sup> & 3 <sup>rd</sup> Floor: -			

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# International Research Journal of Engineering and Technology (IRJET) e-ISSN: 2395-0056

Volume: 06 Issue: 04 | Apr 2019

www.irjet.net

p-ISSN: 2395-0072

Load from upper floor=170.25 KN

- Roof slab = 10.89 x 12.75
  - = 138.85 KN
- Walls = 2.86 x 11.52 = 32.95 KN
- Main Beam = 2.495 x 4.71 = 11.75 KN
- Secondary Beam = 3.21 x 6.0375 = 19.38 KN
- Total Load = 202.93 KN
- 3. <u>3rd & 2nd Floor</u>:-

Load from upper floor=373.18 KN.

- Floor slab = 138.85 KN.
- Walls = 32.95 KN.
- Main beam =11.75 KN.
- Secondary beam = 19.38 KN.
- Total load = 576.11 KN.
- 4. <u>2<sup>nd</sup> & 1<sup>st</sup> Floor</u>:-

Load from upper floor = 576.11 KN.

- Floor slab = 138.85 KN.
- Walls = 32.95 KN.
- Main beam =11.75 KN.
- Secondary beam = 19.38 KN.
- Total load = 779.04 KN.

5. <u>1<sup>st</sup> Floor & Plinth</u>:-

- Load from upper floor = 779.04 KN.
  - Floor slab = 138.85 KN.
  - Walls = 32.95 KN.
  - Main beam =11.75 KN.
  - Secondary beam = 19.38 KN.
- Total load = 981.97 KN.
- 6. <u>Column Between Plinth and Footing</u> :-

• Load from upper floor = 981.97 KN Assume no floor slab at plinth and consider only plinth beam and no walls.

- Wt. of main beam = 11.75 KN
- Wt. of complete column
- =[3+3.04+3.04+3.04+3.04+3.04] x (0.2 x 0.61) x 25= 63.83KN
- Total load = (981.95+63.83) = 1045.78KN.

# Design of column at ground floor :

 $P_{\rm U} = 981.95 \text{ KN} \sim 982 \text{ KN}$ 

 $M_{ux} = 15 \text{ KN.M}$  (assume)

M<sub>uy</sub> = 11 KN.M (assume)

Size of column =  $(230 \times 450)$  MM

Effective length = 60 MM

b = 230 MM , D = 450 MM & d' = 60 MM

Max<sup>m</sup> unsupported length of column

l = 3.04 - (0.450/2) - 0.45/2 = 2.59 M

Effective length (IS 456-2000, P.N 94, T-28)

 $L_{eff} = 0.65l = 0.65 \text{ x } 2.59 = 1.68 \text{ M} = 1680 \text{ MM}$ 

 $L_{ex}/D = 1680/450 = 3.75 > 12$ 

L<sub>ey</sub>/b = 1680/230 = 7.30 >12 [IS:456-2000 Pg.No-42]

 $L_{\text{ex}}/D\,$  &  $L_{\text{ey}}/b$  is less then 12 then than Assume short column.

::consider as short column.

#### Selecting trial section :

P<sub>u</sub> = 982 KN M<sub>u</sub> =  $1.5\sqrt{Mux^2 + Muy^2}$ =  $1.5\sqrt{20^2 + 18^2}$ = 30.49 KN.M d'/D = 60/450 = 0.133 ≈ 0.1

$$Pu /Fck.b.d = (30.49 \times 10^6) / (20 \times 230 \times 450^2)$$

= 0.033

P/Fck = 0.02

 $P = 20 \ge 0.02 = 0.4\%$ .

 $ASC = 0.4 \times 230 \times 450 = 414 \text{ MM}^2$ 

Provided = 6#12MMØ [678.58MM<sup>2</sup>]

Actual Pt % = 678.58 x 100/ (230 x 600)

= 0.65%

#### Checking iteration formula:

 $\left[\frac{Mux}{Mux1}\right]^{\wedge}\alpha_n + \left[\frac{Mxy}{Mxy1}\right]^{\wedge}\alpha_n \le 1$ 

1. <u>To find out Mux<sub>1</sub> :</u>

d'/D = 0.133 ≈ 0.10

P/Fck = 0.65/20 = 0.032

 $Pu/Fck.b.d^2 = 982 \times 10^3/(20 \times 230 \times 450) = 0.474$ 

Mux1/ Fck.b.d<sup>2</sup> = 0.02 [sp.16 P.g N.o – 137]

 $Mux1 = 0.020 \text{ x } 20 \text{ x } 230 \text{ x } 450^2$ 

= 18.63 KN.M

2. <u>To find out Muy</u><sub>1</sub>:

 $d'/D = 60/230 = 0.26 \approx 0.20$ 

P/Fck = 0.65/20 = 0.032

International Research Journal of Engineering and Technology (IRJET) Volume: 06 Issue: 04 | Apr 2019

www.irjet.net

e-ISSN: 2395-0056 p-ISSN: 2395-0072

 $Pu/Fck.b.d^2 = 982 \times 10^3/(20 \times 230 \times 450)$ = 0.474Mux1/ Fck.b.d<sup>2</sup> = 0.02 [Sp.16 pg. No.-137] Muy1 = 0.02x 20 x 230 x 450<sup>2</sup>

= 18.63 KN.M

#### To find out $\alpha_n$ :

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 $Pu/pu_z = \alpha_n$ 

 $pu_z = 0.45$  Fck AC + 0.75 Fy ASC

 $AC = (230 \times 450) - ASC$ 

= 102821.42 MM<sup>2</sup>

$$ASC = 678.58 \text{ MM}^2$$

$$pu_z = (0.45 \times 20 \times 102821.42) +$$

(0.75 x 415 678.58)

 $Pu = 982 \times 10^{3} KN$ 

$$Pu/pu_z = (982 \times 10^3)/(1136.60 \times 10^3)$$

= 0.86

 $\alpha_n = (2 \ge 0.86) = 0.8 = 2.15$ 

$$[\frac{15}{33.12}]^{2.15} + [\frac{11}{33.12}]^{2.15} \le 1$$

::Provided 6#12MMØ [678.58 MM<sup>2</sup>]

#### Lateral ties :

Dia. Of lateral ties (IS 456 – 2000 Pg. NO. 49)

i.  $1/4 \times 12 = 3 \text{ MM}$ ii. 12 MM Provide 8 MM Dia. On Ties.

# Pitch :

Least lateral dimention = 230MM i. ii. 16 x 12 ( dia. Of bar ) = 192 MM

iii. 300MM.

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::Provided 8 MMØ@150 MM c/c.
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Fig2: Loads on Column

# **4.4 STAAD-PRO OUTPUT ANALYSIS**

In our project we considered a G+4 residential building for planning design & analysis. The each floor contents 4 no's of 2BHK flat. Hear we analyses 1 flat area up to the top floor. So staad pro output is on the basis of 1 flat area.



Fig3: Beam no. of ground floor building plan.

Table -1: Detailing of beams

Sr.	Beam	Top bar	Bottom	Spacing of
No	No.		bar	stirrup
1	73,76,77,	2#10mm	2#10mm	2-L
	79,80.81,			8mm@110mm
	82,84,90,			
	91,95,			
	100,106,			
	107,109			
2	74,108,	2#12mm	2#12mm	2-L

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e-ISSN: 2395-0056 p-ISSN: 2395-0072

	98,83			8mm@110mm
3	75,78,85,	2#12mm	2#10mm	2-L
	86.93.97.			8mm@110mm
	102			_
4	87,88,89,	2#10mm	2#10mm	2-L
	92			8mm@200mm
5	94	3#10mm	2#12mm	2-L
				8mm@100mm
6	96,105	4#10mm	2#12mm	2-L
				8mm@110mm
7	101	2#10mm	4#10mm	2-L
				8mm@110mm
8	103	4#10mm	2#10mm	2-L
				8mm@110mm
9	104	2#10mm	2#12mm	2-L
				8mm@110mm
10	110	4#10mm	2#10mm	2-L
				8mm@110mm
11	111	2#10mm	4#10mm	2-L
				8mm@110mm
12	274	2#12mm	2#12mm	2-L
				8mm@200mm



Fig4: 3D render model of building.



**Fig5**: displacement on concrete member.





Fig7: shear forces on member



Fig8: stress on concrete member



International Research Journal of Engineering and Technology (IRJET)e-ISSN: 2395-0056Volume: 06 Issue: 04 | Apr 2019www.irjet.netp-ISSN: 2395-0072



Fig9: Torsion on roof slab

# **5. CONCLUSIONS**

After analysing the G+4 storey building structure, concluded that structure is safe in loading like dead load, live load, wind load and seismic load.

Member dimensions (Beam, Column, Slab) are assigns by calculating the load type and it's quantity applied on it. Autocad plan gives detailed information of the structure members length, height, depth, size & numbers etc.

STAAD PRO has the capability to calculate the reinforcement needed for any concrete section. The program contains a number of parameters which are designed as per IS: 456(2000). Beams are designed for flexure, shear and torsion and its give the detail number, position, spacing of reinforcement.

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