

“EFFECT OF CHANGE IN LOCATION OF ESSENTIAL ELEMENTS OF SADDLE SUPPORTS”

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Abstract – Pressure vessels are subjected to various types of loadings viz. internal / external pressure, operating conditions thermal loadings, nozzle loadings, hydro test pressure, wind and seismic loadings, etc. These loads are transferred to the foundation through saddle supports. Thus, in addition to pressure boundary, one of the important elements in the construction is saddle supports. The structural analysis of supports is being carried out for two configurations and results compared.

Key Words: Pressure vessel, saddle supports, ANSYS, FEA, stress analysis, design of saddle

1. INTRODUCTION

Pressure vessel is an enclosed container in which a fluid, in the form of liquid or gas, is stored under the desired pressure. In addition to the internal pressure, external forces due to wind, seismic, piping, dead loads, etc. are to be considered for design. Furthermore, hydrostatic tests are to be performed at higher pressure to ensure that the pressure vessel could withstand the desired loads. Pressure vessels are supported on support systems, which must withstand the above-mentioned loads. Therefore, stress analysis must be performed on the supports to check the safety of the design. Finite Element Analysis (FEM) enables simulation of the theoretical loads acting on the pressure vessel and thus helps to optimize and validate the design. In the present work, supports were modelled on SOLIDWORKS and the analysis were performed on ANSYS 18.1 simulation software.

2. LITERATURE REVIEW

L. P. Zick (1951)[1] presented a study in which he discussed various stresses acting in cylindrical vessels. Using these stresses, it is possible to determine which pressure vessels must be designed only based on internal pressure. It also helps to develop stiffening rings for those requiring it.

Shen Naijie (1995)[2] found out the stresses in the saddle supports of pressure vessels by experimental and theoretical analysis, using electric strain gauge and double Fourier series expansion method. Also, a trial and error method has been proposed to determine the contact pressure distribution pattern.

N.EL-Abbasi(2001)[3] In this research, a three-dimensional finite-element analysis of the pressure vessel resting on a

flexible saddle framework was created. It evaluates and addresses the effects of saddle length, saddle width, plate extension, and support overhang on the resulting stress fields in the vessel and the support.

Shafique M. A. Khan (2010)[4] The stress distribution was discovered in various parts of the saddle, such as wear, network, flange and base plate, using 3D finite element analysis. Based on the optimum values of the support distance ratio from the end of the vessel, the effects of load shift and various geometric parameters were studied, and recommendations were made.

3. DESIGN OF PRESSURE VESSEL AND SADDLE SUPPORTS

The design of pressure vessel were carried out on Solidworks and analyzed on ANSYS.

3.1 Design of Pressure Vessel

The pressure vessel considered in our analysis is meant to carry LPG as its working fluid, with the following general dimensions-

Table -1

Dimensions of pressure vessel	
Shell outside diameter, D	2133.6 mm
Shell length L	5000 mm
Spherical head outside diameter	2133.6 mm
Corrosion allowance	1.28 mm
Thickness	91.8 mm

The material used for pressure vessel and saddle is SA-516 GR. 70 with the following properties –

Table -2

Properties of Saddle Material	
Material	SA-516 GR.70
Density	7750 kg/m ³
Modulus of Elasticity	1.92E+11 N/m ²
Poisson ratio	0.3
Yield Strength	260 MPa
Operating pressure	1.69 MPa
Design Pressure	6.8 MPa
Operating temperature	297 K

The design, cross section and model of the pressure vessel are as shown below -

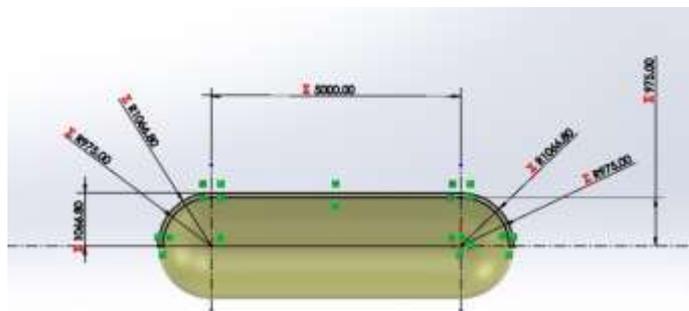


Fig -1: Dimensions of CAD model of pressure vessel

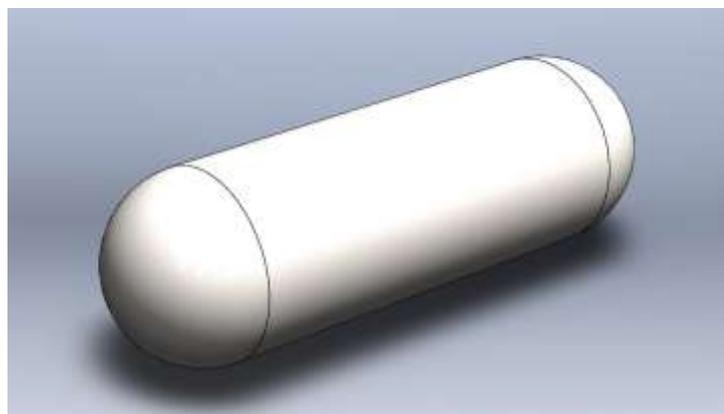


Fig -2: CAD model of pressure vessel

3.2 Design of Saddle

The dimensions for saddle were taken from the Dennis Moss book (2013)[5].

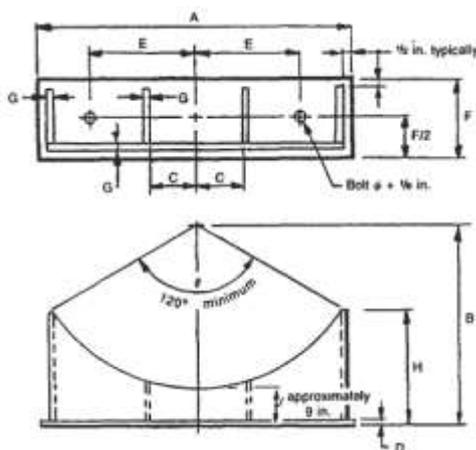


Fig -3: Saddle Dimensions

Typical Saddle Dimensions

Vessel O.D.	Maximum Operating Weight	A	B	C	D	E	F	G	H	Bolt Diameter	Approximate Weight/Set
24	15,400	22	21	N/A	0.5	7	4	0.25	10.2	1/2	85
36	16,700	27	24			9	4		16.5	1/2	100
36	15,700	33	27			12	6		18.8	1/2	179
42	15,100	39	30			15	6		20.0	1/2	209
48	20,200	44	33			18	8		22.2	1/2	280
54	24,700	48	36			20	8		23.7	1/2	373
60	36,500	54	39			23	10		25.0	1/2	510
66	38,800	60	42			26	10		27.2	1/2	563
72	50,700	64	45	10	0.75	29	10	0.375	27.6	1/2	620
78	58,000	70	48	11	0.75	31	8		28.8	1/2	710
84	67,825	74	51	12		33	8		30.2	1/2	810
90	84,200	80	54	13		36	10		32.3	1/2	880
96	92,400	86	57	14		39	10		34.7	1/2	940
102	94,500	92	60	15		42	10	0.500	37.0	1/2	1,360
108	85,800	98	63	16		44	10		37.3	1/2	1,400
114	99,800	102	66	17		47	10	0.625	39.6	1/2	1,780
120	100,000	108	69	18		49	10		40.0	1/2	1,800
130	177,000	118	75	20		55	10		44.5	1/2	2,160
144	200,000	128	81	22		60	10		47.0	1/2	2,320
156	286,000	140	87	24		66	10		51.0	1/2	3,730

*Table is in inches and pounds and Approx.

Fig -4: Typical Saddle Dimensions

Based on the above table, we have selected 84-inch diameter pressure vessel and designed the saddle according to the dimensions given. In order to have further clarity, the table given below has been prepared-

Table -3

Typical Saddle Dimensions	
Vessel O.D.	84 inches
Maximum Operating Weight	57525 pounds
A	74 inches
B	51 inches
C	12 inches
D	0.75 inches
E	33 inches
F	8 inches
G	0.375 inches
H	30.2 inches
Bolt Diameter	1.25 inches
Saddle Angle (θ)	121 \square
Approximate Weight / Set	810 pounds

The saddle modeled in Solidworks is as shown below.

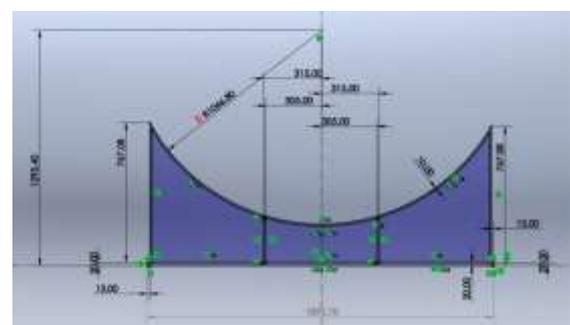


Fig -5: Dimensions of saddle in CAD

3.3 Forces and Boundary Conditions

The forces considered for analyzing the saddle are as follows-

i) Gravitational Force

The primary force that a saddle has to bear is the force due to its own weight. The mass of the saddle came out to be 237 kg.

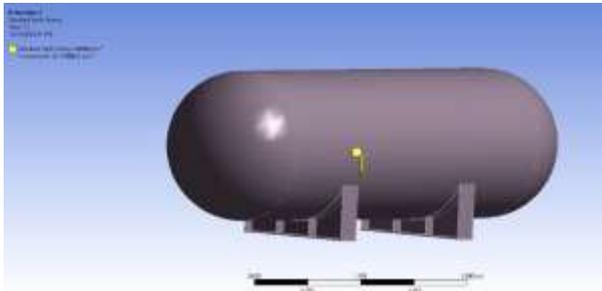


Fig -6: Gravitational force

ii) Pressure Force

The pressure vessel was designed for operating at 1.69 MPa pressure. The force due to the expansion of the vessel due to the internal pressure acts on the saddle.

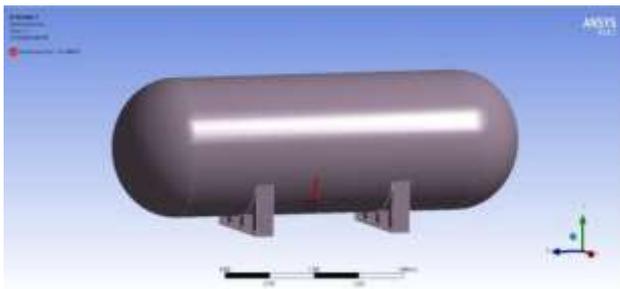


Fig -7: Pressure Force

iii) Wind Loads

Wind load was calculated for the Zone-4 structure in India, which came out to be 20 kN in longitudinal direction and 5 kN in lateral direction.

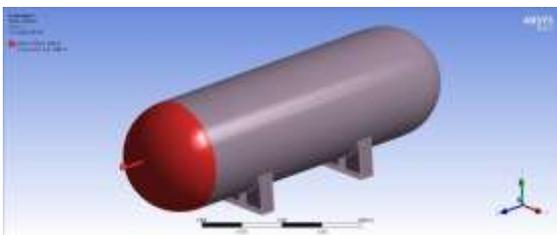


Fig -8: Wind load in lateral direction

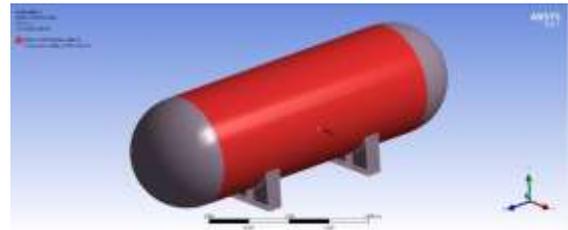


Fig -9: Wind load in longitudinal direction

iv) Constraints

Both of the saddles were fixed at their base to simulate no movement in the saddles.

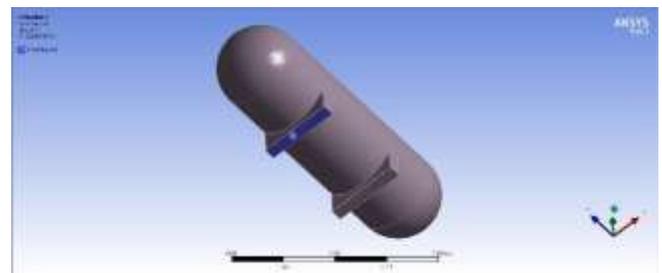


Fig -10: Fixed Support (Saddle 1)

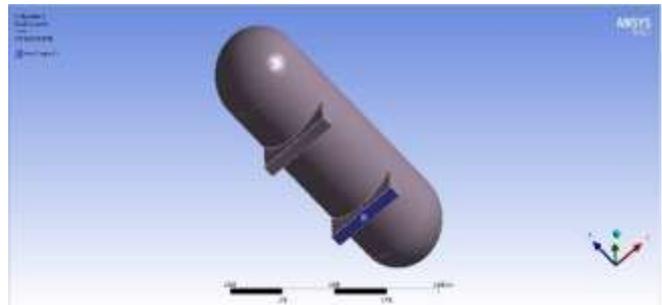


Fig -11: Fixed Support (Saddle 2)

4. ANALYSIS AND ITERATIONS

I) Iteration 1

As the first iteration, the saddle was designed with two vertical ribs on the sides and one web at the centre, which is considered as the baseline design. The saddle and its cross section are shown below.

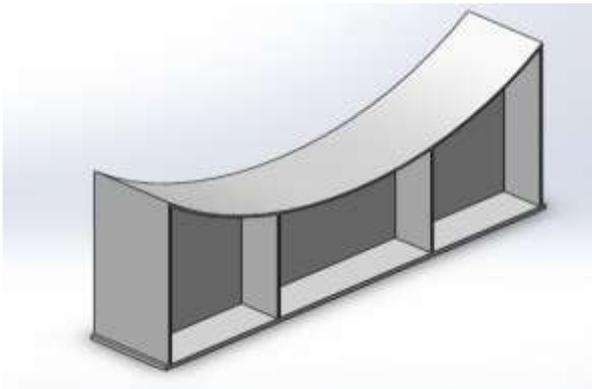


Fig -12: CAD model of saddle (Iteration 1)

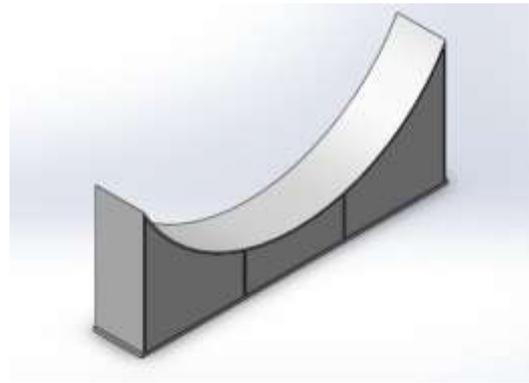


Fig -15: CAD model of saddle (Iteration 2)

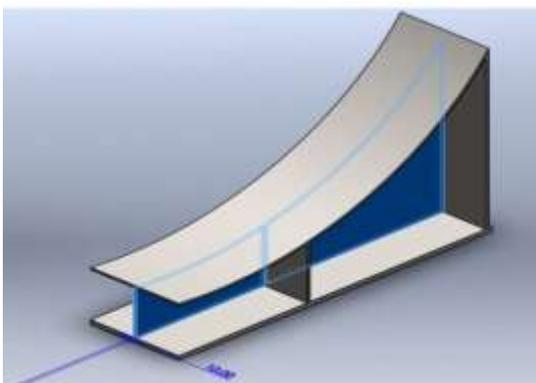


Fig -13: Section CAD model of saddle (Iteration 1)

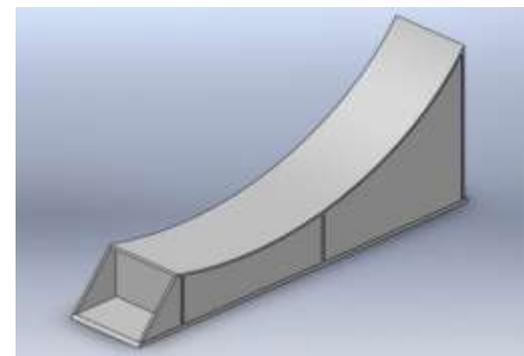


Fig -16: Section CAD model of saddle (Iteration 2)

Analysis of the structure using ANSYS indicated maximum Von Mises stress of 31 MPa in the saddle.

Analysis of this structure indicated maximum Von Mises stress of 36 MPa in the saddle.

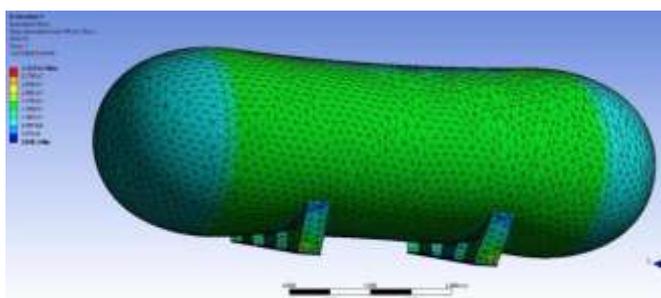


Fig -14: Von Mises Stresses of Iteration 1

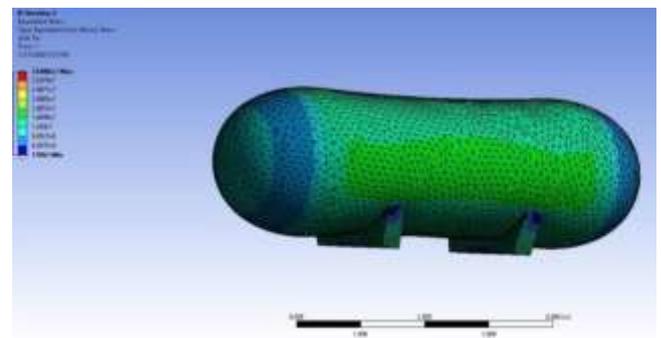


Fig -17: Von Mises Stresses of Iteration 2

II) Iteration 2

In the second iteration, the saddle was designed with two side webs without the inner centre web. The two centre ribs were retained the saddle and its cut section are shown below.

III) Iteration 3

In the third iteration, the saddle was designed with two side webs only, without any ribs. This was like a box type structure. The saddle and its cut section are shown below.

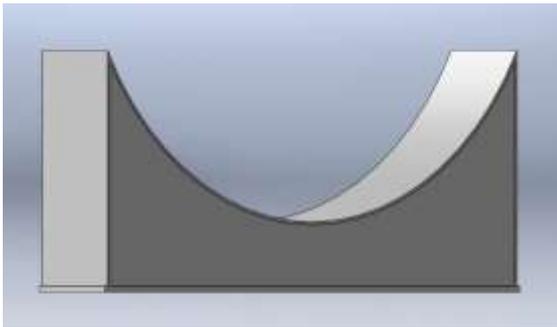


Fig -18: CAD model of saddle (Iteration 3)

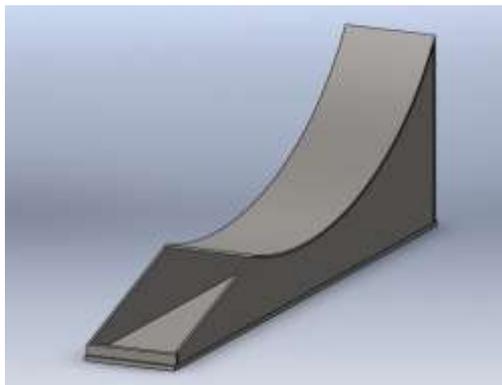


Fig -19: Section CAD model of saddle (Iteration 3)

The maximum Von Mises stress was found to be 40 MPa in the saddle.

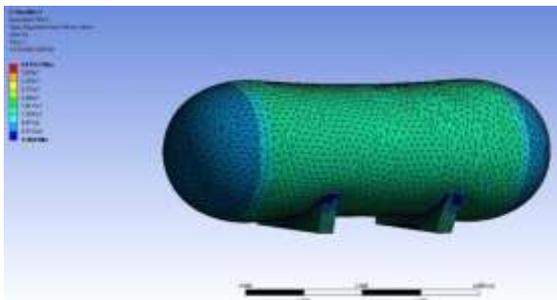


Fig -20: Von Mises Stresses of Iteration 3

5. CONCLUSION

The following are the observations from the ANSYS analysis of different saddles.

Table -4

Saddle Optimization Results		
Iterations	Weight (kg)	Factor of Safety
1 (Baseline)	237	8.39
2	289	7.20
3	279	6.38

As the initial design was over-designed with a factor of safety greater than 8, the design was modified. Although we could reduce the factor of safety to considerable levels, the weight

of the saddle increased in subsequent iterations. Therefore, further modifications are necessary in the design for reducing the weight of the saddle. The modifications can be in the form of providing patterned gaps or holes in the low stressed areas.

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BIOGRAPHIES



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