

Design of Connections in Tubular Structure

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Abstract – Due to advancements in the construction industry a slow shift from RCC structures to steel structures can be seen. Steel tube structures have started dominating construction industry due to its various advantages like they perform better in twisting and minor direction bending capacity, are better in buckling due to less slenderness ratio, provide better earthquake performance, no shuttering is required in composite columns, Less Construction Time is required.

All these members and components are joined by connections, so it becomes important to design the steel junction connections precisely and with utmost care. These connections are responsible for the transference of forces or loads from one member to another. In this project various connection details have been designed manually.

Key Words: Steel connections, Steel tubes, Shear connections, Bolted connection, Fixed welded connection.

1. INTRODUCTION

Connection design is One of the most important components of steel detailing. It is the essential part of the process which makes sure that the components hold together as they probably should. Dy by day Engineers are developing new ideas and coming up with new and improved challenging designs. Without proper connection designs, the completion of new steel tubes building buildings is not possible. The steel framework, which is concealed under a sleek facade, is put to extreme pressures by the building's tall heights and unusual geometries. There is a great demand for precise steel details and connection design.

Producing steel detailing and connecting designs is a difficulty for all buildings, of course. It is also important for less complex construction projects, such as factory structures, apartment complexes with distinctive balconies, and bridges. To ensure that lives aren't put in danger, they all need precise, dependable steel details and connection design

Fundamentally , the connectivity element of steel detailing is what is used to calculate the transference of forces between sections of steel. Basically, these forces can be categorised into : Beam to beam, bracing connections, column to beam, and splice.

A connection must be designed for connectivity in order to assure that it won't fail due to the applied load detail. It must also take into account the requirements of fabricators and erectors while creating and putting in place the various components. The method of verifying steel connections must include demonstrating the quality of welds and confirming that the stresses placed on the steel plates, sections, and bolts holding them together are all well within the tolerances of the materials that are specified.

1.1 TYPES OF CONNECTIONS

On the basis of different loads broadly steel connections can be categorized into following types.

- 1.Tension Connections
- 2.Compression Connections
- 3.Shear Connections
- 4.Moment Connections

Steel connections can further be classified on the basis of the restraint they provide. These classifications (in decreasing restraint level are as follows:

- 1.Fully restrained moment connections
- 2.Partially restrained moment connections
- 3.Simple shear connections

The fully restrained connections can resist the maximum end moments and it allows minimum amount of end rotation while as simple shear connections supports lower end moments and allows maximum end rotation. Partially restrained connections lie in the middle of fully restrained and the simple shear connections

2. AXIAL CONNECTON FOR BRACINGS

Grade of Steel, fy	= 345 N/mm ²
Details of Section (D x B x t)	= 250x250x10mm ³
Area of Section, Ag	= 9600 mm ²
Diameter of Bolt	= 24 mm
Grade of Bolt	= 8.8
No. of Bolts Provided	= 18 Minimum 31 Bolts
No. of Bolts Provided along Width of Plate	= 3
Provided Thickness of Plate	= 32 mm

2.1 Welded connection for bracing

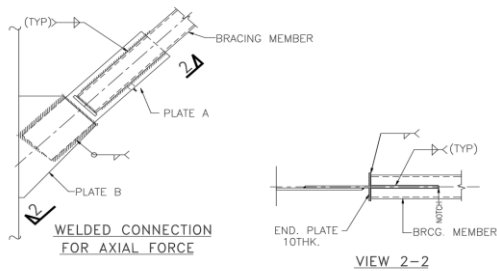


Fig -1: Typical detail for welded bracing connection

As per is 800 2007 connection should be designed for tension force of $1.2 \times A_g \times F_y$

$$\begin{aligned} \text{Tensile force for connection} &= 1.2 \times A_g \times F_y \\ &= 1.2 \times 9600 \times 345 \\ &= 3974.4 \text{ kN} \end{aligned}$$

Taking Plate Strength T_{dg} = Tensile force for connection
 $0.9 \times (\text{Width of plate}) \times (345/1.25) \times 32 = 3974.4 \text{ kN}$
 So, Required Width of plate A adjacent to plate B = 500mm

Plate to Gusset Plate Connection (Welding Required)

$$\begin{aligned} \text{Provided Weld Thickness} &= 32 \times 0.7 = 22 \text{ mm} \\ \text{Length of Weld} &= \frac{\text{Area of Weld}}{\text{Weld Thickness}} \end{aligned}$$

$$\begin{aligned} \text{Area Of weld between plate A and B} &= 3974.4 \times 10^3 \times \sqrt{3} \times 1.5/345 = 29929.8 \text{ mm}^2 \\ \text{Length of Weld} &= 29929.84/22 = 1426 \text{ mm} \end{aligned}$$

$$\begin{aligned} \text{Length of Weld except on width of plate} &= 1426 - 500 = 926 \text{ mm} \\ \text{Length of Weld on one side} &= 926/2 = 463 \text{ mm} \end{aligned}$$

2.2 Bolt connection

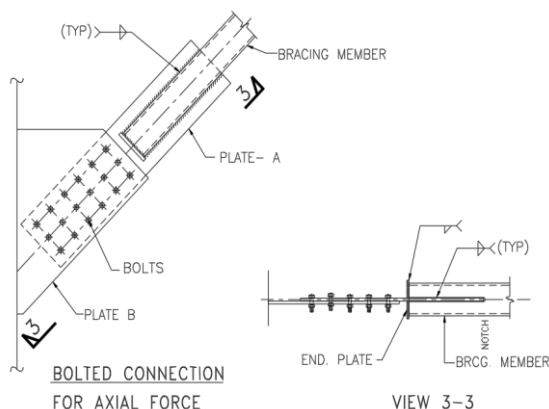


Fig -2: Typical detail for bolted bracing connection

Tensile force for connection = 3974 kN
 Shear Capacity of Bolt

$$= \frac{f_u}{\gamma_{m1}} \times A_{nb} \times \sqrt{3}$$

$$\begin{aligned} A_{nb} &= \text{Net area of bolt} = 0.78 \times \text{area of shank} \\ &= 800/125 \times 352.86/\sqrt{3} = 130.38 \text{ KN} \\ \text{No. of Bolts required} &= 3974.4/130.38 = 30.48 \gg 31 \end{aligned}$$

$$\begin{aligned} \text{Area of weld between member and plate A} &= 3974.4 \times 10^3 \times \sqrt{3} \times 1.5/345 \\ &= 29929.8 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} \text{Allowable weld on member} &= 0.7 \times 10 = 7 \text{ mm} \\ \text{Length of weld} &= 29929/(7 \times 2) = 2137 \text{ mm} \\ \text{Length of weld on both side of member} &= 2137/2 = 1068 \text{ mm.} \end{aligned}$$

2.3 Shear connection for secondary beams

Section Details (DxBxt)	= ISMB350
Grade of Steel	= 250 N/mm ²
Diameter of Bolt	= 16 m
Grade of Bolt	= 8.8
No. of Bolts Provided	= 4
Pitch Distance of Bolts, p	= 75 mm
Edge Distance of Bolts, e	= 50 mm
Thickness of Plate	= 25 mm
Thickness of Weld	= 8.5 mm

FOR SHEAR FORCE

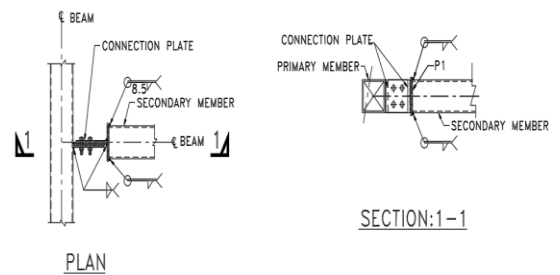


Fig -3: Typical detail for bolted shear connection

Loads on floor

$$\begin{aligned} \text{Self-weight of deck slab} &= (0.080 + 0.0375) \times 25 + 0.001 \times 78.5 = 3.016 \text{ kN/m}^2 \\ \text{Floor finish} &= 0.05 \times 25 = 1.25 \text{ kN/m}^2 \end{aligned}$$

$$\begin{aligned} \text{Service load} &= 1 \text{ kN/m}^2 \\ \text{Partition wall load} &= 1 \text{ kN/m}^2 \\ \text{Live load} &= 3 \text{ kN/m}^2 \\ \text{Total load} &= 9.266 \text{ kN/m}^2 \end{aligned}$$

Contributory width of deck slab = 2m
 UDL on secondary beam = 18.532 kN/m2
 Total factored shear at support = $1.5 \times 7.5 \times 18.532 / 2$
 = 105 KN

Bolted Connection

Shear Capacity of Bolt, V_{nsb}
 = $(f_u \times n_n \times A_{nb}) / \sqrt{3} \gamma_{mb}$ = $(800 \times 1 \times 157) / \sqrt{3} / 1.25$
 = 58 kN

No. of Bolts Required = $105 / 58$
 = 1.8

Provided No. of Bolts = 4

Check plate strength –

Distance of 1st row of bolt from member = 75 mm

Distance of 2nd row of bolt from member = 150mm

Moment at main member face
 = $0.075 \times 105 \times 0.5 + 0.15 \times 105 \times 0.5 = 11.82$ kNm

Assume 12mm thk. Plate

Moment capacity of plate = $Z_e F_y / \gamma_{mo}$
 = $bd^2 / 6 \times 350 / 1.1$
 = 11.82 KNm

d (depth of plate) = $\sqrt{((11.82 \times 10^6 \times 1.1 \times 6) / (12 \times 350))}$
 d = 136 mm

Provide 350 mm deep plate

Bending capacity of 350 mm deep plate = $Z_e F_y / \gamma_{mo}$
 = $(12 \times 350^2 \times 350) / (6 \times 1.1) = 78$ KNm

Shear strength of plate = $A_g F_y / \gamma_{mo}$
 = $12 \times 400 \times 350 / 1.1$
 = 1336 KN

Now combined ratio in axial and bending

$N/N_d + M/M_d \leq 1$

Here N = 1.5 KN M = 11.82
 N_d = 1336 KN M_d = 78
 = $1.5 / 1336 + 11.82 / 78 = 0.23 \leq 1$

Safe

Check welding of connection plate to primary member

Provide thickness of weld = 6mm on each side
 Shear stress in weld = $(105 \times 1000) / (6 \times 350 \times 2)$
 = 25 N/mm²

Section modulus of weld = $bd^2 / 6$
 = $(6 \times 350^2 \times 2) / 6$
 = 245000 mm³

Bending stress in weld = $(11.82 \times 10^6) / 245000$
 = 49 N/mm²

Equivalent stress, F_e = $\sqrt{(f_a^2 + 3q^2)} \leq f_y / (\sqrt{3} \gamma_{mw})$
 $f_a = 49$ N/m² = $\sqrt{(49^2 + 25^2 \times 3)} \leq 490 / (\sqrt{3} \times 1.25)$
 $q = 25$ N/mm = 66 N/mm² ≤ 226 N/mm²

Safe

2.4 Fixed Bolted Connection Detail for main beam to main beam (on view 5-5 in figure)

Moment, M (From Etab) = 292 kNm
 Shear, V (From Etab) = 242 kN
 Diameter of Bolt = 20 mm
 Grade of Bolt = 10.9
 Grade of Steel Plate = 350 N/mm²
 Plate Details (DxB) = 400 X 600 mm²
 Depth of Stiffener above or below member = 100 mm
 Distance Between Stiffener plates = 100 mm

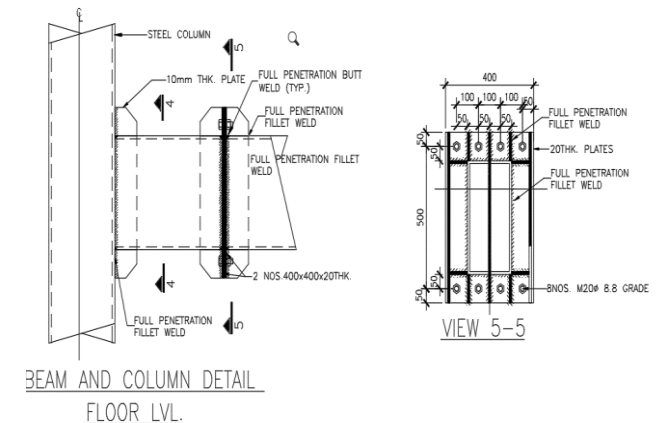


Fig -4: Typical detail for bolted tube splice connection

Distance between upper bolt row and lower bolt row = 500 mm

Tension in Extreme Bolt, T = $292 / (0.5 \times 0.4)$
 = 146 kN

Shear in each bolt = $242 / 8$
 = 30.25 kN

Tension Capacity of Bolt = $0.9 \times 0.78 \times 314.16 \times 1000 / 1.25$
 = 176.43 kN

Shear Capacity of Bolt = $1000 \times 0.78 \times 314.16 / (\sqrt{3} \times 1.25)$
 = 113.18 kN

Combined Shear and Tension = $(146 / 176.43)^2 + (30.25 / 113.1)^2$
 = $(0.83)^2 + (0.27)^2$
 = 0.76 < 1

Connection is SAFE

Design of Plate at View 5-5

Moment due to Tension in bolt = $w \times l / 8$
 = $146 \times 0.1 / 8$
 = 1.83 kNm

Thickness of Plate = $1.2 \times (100 - 22) \times d^2 / 6 \times 350 / 1.1$
 Now, Thickness of plate Calculated from = 1.83 kNm
 = 1.83×106

= $1.2 \times (100 - 22) \times d^2 / 6 \times 350 / 1.1$
 d² = 368.6813187
 = 20 mm

2.5 Fixed Welded Connection Detail

On view 4-4 in figure -

Grade of Steel, f_y	= 350
Ultimate Strength of Steel, f_u	= 490 N/mm ²
Section Details (DxBxt)	= 400x200x10
Area of Cross Section, A	= 116 cm ²
Elastic Section Modulus, Z_e	= 1217.9 cm ³
Plastic Section Modulus, Z_p	= 1502 cm ³
Shear from Etabs, V	= 252 kN
No. of Stiffeners on one side of member	= 3
Depth of Stiffener above and below member	= 100 mm

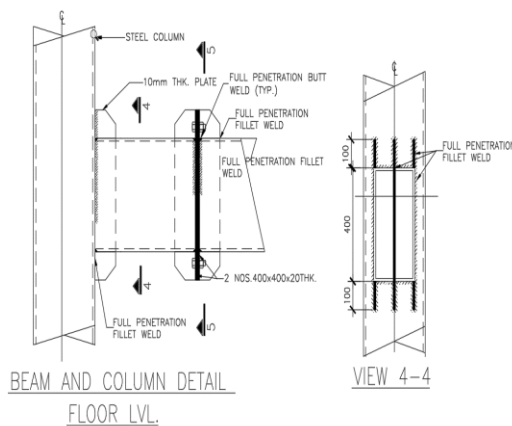


Fig -4: Typical detail for welded tube column beam junction connection

As per IS 800 -2007 all column beam junction should be designed for 1.2 times plastic moment capacity

Design Bending Strength of Steel Beam, M_d	
$= \beta_b \times Z_p \times f_y / \gamma_{mo} \times 1.2$	
$= 1.2 \times 1502000 \times 350 / 1.1$	= 573.49 kNm
Shear force at face of column	= 252 kN
Assumed Height of Stiffener (View 4-4)	= 100 mm
Area of weld for shear	$= (400 + (200 \times 3)) \times 2 \times t_e$
	= 2000 t_e

Moment of Inertia of weld	
$= (t_e \times 400^3) / 12 \times 2 + (600 \times t_e) \times 250^2 \times 2 + (t_e \times 100^3) / 12 \times 12 + (200 \times t_e) \times 200^2 \times 2$	
$= 10666666.66 t_e + 75000000 t_e + 999999.96 t_e + 16000000 t_e$	
	= 102666666.6 t_e

MOI of Weld	= 102.67 $\times t_e \times 10^6$ mm ⁴
Section Modulus of weld, Z	= 102.67 / 300 $\times t_e$
	= 34 $\times t_e \times 10^4$ mm ³

Moment/ Section Modulus, M/Z	
$= (292 \times 10^6 \text{ Nmm}) / 34 \times 10^4 \text{ mm}^3 t_e$	
	= 858.8235294 / t_e N/mm ²

Shear Stress	= 252 $\times 10^3 / 2000 t_e$
	= 126 / t_e N/mm ²

Equivalent Stress, f_e	= $\sqrt{f_a^2 + 3q^2}$
Now, f_a	= 858.8235294 / t_e

q	= 126 / t_e
$f_e = \sqrt{858.8235294^2 + (3 \times 126^2)} / t_e$	
Equivalent Stress, f_e	= 886.1184202 / t_e
Equivalent Stress, f_e	= 490 / (($\sqrt{3}$) $\times 1.5$)
	= 188.6
So,	= 886.1184202 / t_e
	= 188.6
t_e	= 4.7 mm
Provide throat thickness	= 5mm
Required Thickness of weld	= 5 / 0.7
	= 7.1 mm

3. CONCLUSIONS

Design of steel connection requires vigorous calculations but provides much more control than connection by other building materials.

Upon experience we have understood that steel connection is much more safer than RCC connection.

Any two steel members can be joined by many numbers of connection possibilities as can be seen by the literature above.

The need to calculate modular ratio (m) becomes nil when two members of same material like steel are connected.

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